Lean Concretes Using Kentucky’s Dense Graded Aggregate (Portland Cement and SS-1 Emulsified Asphalt)

James H. Havens*  Milton Evans Jr.†
MEMO TO: D. V. Terrell
Director of Research

The attached report, "Lean Concretes Using Kentucky's Dense-Graded Aggregate (Portland Cement and SS-1 Emulsified Asphalt)", represents a laboratory investigation on the effects of the 2 cements on dense-graded aggregate.

I believe, with the design data and particularly mixture properties as shown in this report, that we should proceed with plans to build a test pavement incorporating at least these 2 cementing agents. The treated dense-graded aggregate should be evaluated as a base type. It may have merit for a component of high type shoulder construction.

We are studying with interest the use of slip form pavers for placing portland cement treated dense-graded aggregate base courses.

Respectfully submitted

W. B. Drake
Associate Director of Research

WBD:dl
Enc.
cc: Research Committee members
    Bureau of Public Roads
LEAN CONCRETES USING KENTUCKY'S DENSE GRADED AGGREGATE
(Portland Cement and SS-1 Emulsified Asphalt)

by

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INTRODUCTION

Since the development of dense-graded aggregate base in Kentucky about 1952 (1)(2)(3), there have been various conjectures about "auto-cementations" or "setting" of these materials when compacted and cured (4)(5). In some cases, particularly when the material was limestone, they have developed rather surprising strengths, in the field as well as in the laboratory. Such displays of strength seem to be directly associated with curing (slow drying) and the possibility of re-deposition of small amounts of dissolved calcium carbonate as cement. If this is so, it might be surmised that bases which have not been "fixed" by curing and drying before surfacing may never acquire strength by virtue of auto-cementation, or may loose it on re-wetting. It may be surmised, likewise, that unless auto-cementation occurs, the supporting ability of the base must be governed by the binding power of whatever moisture is present and by virtue of physical confinement. Thus, the idea of deliberately introducing cement is quite logical if inherent strength is to be assured.


(2) "Report No. 1 on a Water-Bound Dense-Graded Aggregate Base, Casey County Project F 505(1), Phil-Pine Grove Road", by E. G. Williams, Reports of the HMRL, Vol. VIII, Part III, p 286-308, 1953.


The desirabilities of dense-graded aggregate are evident in the ease with which it is manipulated, placed, compacted, shaped, and smoothed to grade. When properly confined above and below and at the sides, as in a base overlain by significant thicknesses of pavement, there seems to be little, if any, need for cemented-strength. However, inherent or cemented strength may be essential where not overlain by significant thicknesses of other pavement. For instance, considerable thought has been given to the possibility that stabilized (cemented) dense-graded aggregates, with or without light surface treatment, might serve as paving system for shoulders on interstate roads and possibly as initial treatments or bases on some rural and secondary roads.

With these possibilities in mind, a series of exploratory experiments were performed in the laboratory on various blends of portland cement (Type I) and dense-graded aggregate and on blends of asphaltic-type cements (SS-1) and dense-graded aggregate. The first objective, of course, was to delineate basic principles in the design of such mixtures and to examine any extraneous factors that may be involved. The Division of Materials made a rather extensive study of SS-1 mixes and a preliminary series of tests on portland cement mixes. This report is, therefore, supplementary to that priority.

In the work reported here, it was presumed that SS-1 was the type of asphaltic material most amenable to use with dense-graded aggregate, that the materials could be best blended by plant mixing,

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and that the mixture would be placed with pavers or by blade-spread-
ing and rolling. It was also presumed that the portland cement blends
would be plant mixed. However, two possibilities existed for the method
of placement. For instance, it would be desirable in many respects to
also place portland cement mixes with a paver (7) or by blade spread-
ing and rolling (compaction at or near optimum moisture content). Al-
ternatively, portland cement blends might well be placed as normal
"slump" concrete. The later method, of course, would probably re-
quire the use of conventional forms. Thus, two types of portland cement
blends needed to be investigated.

It is of interest, of course, from a more general point of view to
compare the present idea, at least in principle, with those of soil-
cement stabilization, bituminous stabilization of fine-grained and
granular soils, as well as lean concretes. In particular, lean concretes
using normal coarse aggregates and otherwise conventional mixture
designs, air-entrainment, slump, etc., offer a third possibility for
base construction. Although a detailed comparison of these is some-
what beyond the scope of this report, it may suffice here to call atten-
tion to the fact that most soils may be successfully stabilized with
5-15% portland cement by volume (5-15% x 27 ft³ = 1.35 to 7.5 sacks/
yd³). Thus, the cement requirements for lean concretes whether made
with DGA or possibly No. 36 stone and sand may be comparable to that
required to stabilize the better graded soils. In 1950, an experimental

(7) As a matter of interest, attention is directed to: "Traveling Forms
for Paving...", Fred F. Loy, District Engineer, Portland Cement
lean concrete base was constructed on US 60, Winchester-Mt. Sterling (8)(9), which used the following mix-design factors:

- Cement factor: 3.5 sacks/yd³
- Ratio of FA to total: 34-38%
- Max. free water: 9.75 gal/sack
- % air: 3 to 6
- Type cement: I-A
- CA: No. 36 limestone
- FA: O.R. sand

The average mix-water during construction was 8.5 gal/sack. Flexural strengths and compressive strengths (28-days) averaged somewhat higher than 400 psi and 1800 psi respectively.

VOLUMETRIC CONSIDERATIONS IN DESIGN

Dense-graded aggregate is normally compacted to 85% solid volume (62.4 x 2.72 = 171 lbs/ft³; 171 x 85% = 145 lbs/ft³ compacted unit dry wt). Usually about 5-1/2 to 6% water (or liquid such as SS-1 or SS-1 plus water) by weight of dry aggregate is optimum for compaction (145 x 6% = 8.7 lbs H₂O; 8.7/62.4 = .14 ft³). At 85% solid volume of aggregate, 0.15 ft³ of bulk cement would be indicated as the maximum allowable assuming that no bulking occurs (0.15 ft³ x 0.48 ft³ solid vol. per sack of cement = 0.072 ft³; 0.85 ft³ + 0.072 ft³ = 92.2% solid vol. of aggregate + cement; 0.15 x 27 = 4.05 bags/yd³ C.F.; and 7.8% water by vol. or 0.078 ft³ x 7.48 gal/ft³ = 0.584 gal/ft³; 0.584 x 27 = 15.7 gal/yd³ or 3.9 gal/sack of cement). However, the optimum


water for compaction remains approximately constant (about 5-1/2 to 6%) regardless of the cement factor. Likewise, water requirements for workability (slump) remain fairly constant (about 35 gal/yd$^3$) regardless of cement factor ($35 \text{ gal/} yd^3 \div 4.05 = 8.65 \text{ gal/sack of cement}$). Thus, 15.7 gal/yd$^3$ is approximately half the amount needed for optimum compaction, and this amount is only 5 to 10 gal/yd$^3$ short of the amount needed for slump consistency. To include the additional amounts (15 to 25 gal.) required by these conditions would involved bulking and increased yields.

**Design by Moisture-Density Tests**

Alternatively, if 5-1/2 to 6% (say 5.75%) water by weight of dry aggregate is assumed or established by moisture-density tests and 146 lbs/ft$^3$ is assumed to be an approximate dry unit weight (based on $SP\ G$ of limestone aggregate as 2.72 and cement as 3.14, total dry wt/yd$^3$ of 4000 lbs; 3-1/2 bag mix; avg. $SP\ G = \frac{339}{4000} \times 3.14 + \frac{4000-339}{4000} \times 2.72 = 0.258 + 2.49 = 2.75), 146 \times 5.75\% = 8.4 \text{ lbs water/} ft^3 \text{ or } 8.4/62.4 = 0.135 \text{ ft}^3$. Then $0.135 \times 27 = 3.64 \text{ ft}^3$ of water/\text{yd}^3.

$$
\begin{align*}
3.64 \text{ ft}^3 & \text{ water/} \text{yd}^3 \\
+1.57 \text{ ft}^3 & \text{ solid vol. of } 3-1/2 \text{ bag cement} \\
+0.41 & \text{ vol. void assuming } 1.5\% \text{ air, entrapped} \\
+0.62 \text{ ft}^3 & \text{ vol. water, cement, and air}
\end{align*}
$$

$$
27.00 - 5.62 = 21.38 \text{ ft}^3, \text{ vol. of DGA} \\
21.38 \times 62.4 \times 2.72 = 3620 \text{ lbs DGA/} \text{yd}^3
$$

$$
\begin{align*}
3620 \text{ lbs DGA} \\
+339 \text{ lbs cement} \\
3959 \text{ lbs dry wt/} \text{yd}^3
\end{align*}
$$

$$
\text{Wet weight} = 3959 + 3.64 \times 62.4 = 4186 \text{ lbs} \\
W/C = 3.64 \times 7.48/3.5 = 7.8 \text{ gal/sack} \\
\text{Free water} = 27.2 \text{ gal/} \text{yd}^3
$$
Correction for Air-Entrainment

Theoretically, if it were possible to entrain significant amounts of air in the above mix and to retain it despite compaction, the air (say 1.5% entrapped + 4.5% entrained = 6% total) would displace DGA only (6% x 27 = 1.62 ft³). Since water and cement would give a combined volume of 5.21 ft³,

\[
\frac{5.21 \text{ ft}^3 \text{ water + cement}}{+1.64 \text{ ft}^3 \text{ total air}} = \frac{6.85 \text{ ft}^3 \text{ water + cement + air}}
\]

\[
27.00 - 6.85 = 20.15 \text{ ft}^3 \text{ vol. DGA}
\]

\[
20.15 \times 62.4 \times 2.72 = 3420 \text{ lbs DGA/yd}^3
\]

\[
3420 \text{ lbs DGA/yd}^3
\]

\[
+339 \text{ lbs cement}
\]

\[
3759 \text{ lbs dry wt/yd}^3
\]

Design for Slump

Although the amount of mixing water to produce slump consistency appears to remain fairly constant (30 to 40 gal/yd³) regardless of cement factor, it seems advisable to run a test series on blends of the particular aggregate and at various cement factors and air contents. Yields should be easily calculated by thus fixing the amounts of air, water and cement and finding the volume of DGA by difference.

Design Using Asphal tic Emulsion (SS-1)

A general criterion for design using SS-1 asphaltic emulsion may be derived similarly by slight modification of the Marshall Stability criterion. Presumably, the optimum M.C. of DGA, as determined by Proctor tests is closely analogous to the optimum asphalt content of bituminous mixes as determined by Marshall compaction. While it is recognized that there may be differences between the two
methods with respect to compactive forces and the lubricating characteristics of asphalt cements as compared to water, the asphaltic emulsion (SS-1), which is dilutable with water, would not be expected to inhibit compaction in either method. Thus, an optimum liquid content, whether consisting of plain water, emulsion, or diluted emulsion, may be determined approximately by either method of compaction; and the resulting density of the DGA should approach or equal the 85% solid volume requirement now applicable to DGA.

Assuming, then, that it is desired to prepare a mixture containing 3% base asphalt (SS-1 contains approximately 60% base asphalt and 40% water), the amount of emulsion required would be 3%/0.60 = 5%. Therefore, if 6% liquid is found to be optimum for compaction, it would be necessary to add 1% water to the mixture or else to dilute the emulsion to the extent that: 3%/X = 6%; X = 50% base asphalt; then, 5:60 :: X : 100, and 60X = 50 x 100, X = 83.5% SS-1, and the dilution water = 16.5%.

Actually, it is foreseeable that unless the aggregates were pre-dampened, absorption of water by the aggregate may cause premature breaking of the emulsion and also rob the mixture of free water. Pre-dampening the aggregate would, therefore, enhance the mixing operation, provided, of course, that any free water or surface water on the aggregate is determined, and provided that the total free liquid content does not exceed the indicated optimum.

The maximum asphalt content would be limited by the indicated optimum liquid content for compaction. Optimum asphalt content, however, may be indicated by factors such as resistance to shear,
strength, or stability. Minimum asphalt content may be indicated by some strength test and resistance to soaking in water.

SUMMARY OF LABORATORY WORK ON P.C. MIXES

In anticipation of the possibility of placing and compacting the portland cement mixes at or near optimum moisture content, moisture density curves were derived for dry blends of DGA (10) and cement, in proportions approximating 2-, 3- and 4-bag mixes. By Proctor compaction, the indicated optiums ranged between 5.5 and 6.0% and by Marshall compaction were between 5.0 and 6.0%. Attempts to prepare test beams and cylinders by ramming and tamping these mixtures into molds were rather unsuccessful. Even though considerable effort was devoted to this part of the work, the specimens so prepared were usually honeycombed and rather un-uniform; and in no case was it possible to produce a troweled finish on them. Although, several such mixes were prepared; it was not possible to evaluate them reliably in terms of beam and cylinder strengths or by F & T durability.

Alternatively, it was found that satisfactory specimens could be prepared by ramming and tamping (Figs. 1 & 2) at water contents considerably higher than optimum but slightly lower than that necessary to give impending slump. This, essentially, was the method used to prepare the zero- or no-slump concretes, Series I and III, reported in Table I.

No-Slump, A/E Mixes (Series IV)

Attempts to entrain air in mixes at optimum water contents were altogether unsuccessful. Realizing, then, that there was insufficient free water in the mixes to form air bubbles, water contents were increased to impending slump. Here, small amounts of air could be entrained by the usual method of mixing, but it was usually dissipated after ramming and tamping in the molds. It was subsequently found, however, that by first mixing the cement, water, and air-entraining agent, a foamy slurry could be formed and that much of this air could be retained after mixing with damp aggregate and even after ramming and tamping the concrete in the molds. This, essentially, was the method used to prepare the no-slump, A/E mixes reported as Series IV in Table I.

A/E, Slump Mixes (Series II)

No difficulties were encountered in mixing, entraining air, or in preparing specimens from mixes of normal slump consistency. The water contents used were simply those necessary to give the desired slump. These mixes are reported as Series II in Table I.

Strengths and Durabilities

Both 7- and 28-day flexural and compressive strengths for the four series of mixes are given in Table I. All specimens were moist-cured in the usual way.

For durability testing, beam specimens were moist-cured 14 days, soaked 24 hours, and then subjected to freeze-thaw (ASTM C-291).

In Table I, it is apparent that 2-bag mixes have very low strengths and very little resistance to F & T. Strengths, of course,
Fig. 1: Ramming and Tamping No-Slump, Lean Concrete in Molds.

Fig. 2: Ramming and Tamping No-Slump, Lean Concrete in Molds with Air Hammer.
increase with increased cement factor as expected by the usual concept of the relationship between strengths and cement factor. It is quite obvious, too, that air entrainment is highly essential to F & T durability (also, see Fig. 3) and that 3 bags/yd$^3$ is about the minimum practicable cement factor if F & T durability is to be assured.

Although the calculated values are not given in Table I, it is apparent that the A/E, 3-in. slump mixes, Series II, required approximately 40 gal/yd$^3$ or 9.2\% water by weight. This exceeds the indicated optimum for compaction (without air) by about 3\%; whereas the no-slump, compacted mixes exceeded optimum by 1 to 4\%, but this difference decreases with increased cement factor.
### TABLE 1: TEST RESULTS ON DENSE GRADED AGGREGATE CONCRETE

<table>
<thead>
<tr>
<th>C.F. (bags)</th>
<th>Method of Placement</th>
<th>Slump in.</th>
<th>Unit Wt. (lb/ft(^3))</th>
<th>Unit Wt. Proctor %</th>
<th>Theo. W/C</th>
<th>Actual W/C</th>
<th>F &amp; T Cycles</th>
<th>Flex. Comp.</th>
<th>Cycles to Failure</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>Rammed and tamped</td>
<td>0</td>
<td>2.0 148.0</td>
<td>5.95</td>
<td>12.47</td>
<td>20.10</td>
<td>10</td>
<td>180</td>
<td>266</td>
</tr>
<tr>
<td>3</td>
<td>in place by hand</td>
<td>0</td>
<td>2.3 147.2</td>
<td>5.54</td>
<td>7.99</td>
<td>10.92</td>
<td>29</td>
<td>420</td>
<td>553</td>
</tr>
<tr>
<td>4</td>
<td>a 2-1/4&quot; diameter</td>
<td>0</td>
<td>1.7 149.2</td>
<td>6.46</td>
<td>7.13</td>
<td>8.69</td>
<td>35</td>
<td>640</td>
<td>647</td>
</tr>
<tr>
<td>5</td>
<td>wooden rod</td>
<td>0</td>
<td>1.4 148.8</td>
<td>-</td>
<td>-</td>
<td>6.92</td>
<td>46</td>
<td>713</td>
<td>807</td>
</tr>
</tbody>
</table>

**Notes:**
- All test data represents average of three specimens.
- Aggregate source: Jessamine and Benson, Lexington Series
- Cement: Type I
Fig. 3: Photograph Showing DGA Concrete Specimens in F & T Chamber after about 25 Cycles. Specimens marked 2- and 4-AE are air-entrained concretes containing 2 and 4 bags of Type I cement, respectively. Deteriorated specimens are non-air concretes containing 2 and 3 bags of cement. Note: 2 specimens of non-air concretes containing 4 bags of cement per cu. yd. (center and lower right) remained in relatively good condition at this stage in the testing.
SUMMARY OF LABORATORY WORK ON SS-1 MIXES

It was anticipated that the dominate factor in the evaluation of the SS-1 mixes would be the rate and degree to which curing would progress under various conditions. Likewise, it was expected that "cemented strength" would not be fully manifested until the asphalt had become completely "fixed" by curing and drying. Having once achieved fixation of the asphalt, a high level of strength should persist after re-wetting and soaking. Hence, the primary objective in this phase of the work was to establish the minimum asphalt content and curing that would assure a high order of strength and water-resistance.

Preliminary Curing Tests

Marshall-type specimens were prepared using 2, 3, and 4% SS-1 and enough water to provide a total liquid content of approximately 6% (approximately optimum). These specimens were cured in various ways and then tested for stability. The data derived therefrom are summarized in Table 2, and it is apparent therein that those curing conditions most favorable to drying resulted in the highest stabilities. It is also apparent that with increasing asphalt contents there was a commensurate loss in stability. While the losses there may be related to the fact that higher percentages of asphalt emulsion would require more rigorous curing in order to impart ultimate strength to the specimens, it is generally understood that this type of loss is characteristic of mixes having asphalt contents higher than optimum. This point of view would indicate that optimum would be rather close to 2%. However, from the standpoint of resistance to water, asphalt contents between 2 and 3% may prove to be more advantageous.
<table>
<thead>
<tr>
<th>Curing Condition</th>
<th>% SS-1 Added</th>
<th>M.C. as Tested</th>
<th>Stability (lbs.)</th>
<th>Flow</th>
<th>Dry Density lbs/ou.ft.</th>
<th>% Voids Total mix</th>
<th>% Voids Agg. Only</th>
<th>% Voids Filled W. App.</th>
</tr>
</thead>
<tbody>
<tr>
<td>In molds 1 day at room temp., tested at room temp.</td>
<td>2</td>
<td>1027</td>
<td>23</td>
<td>142.3</td>
<td>14.2</td>
<td>16.0</td>
<td>16.0*</td>
<td></td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>1200</td>
<td>22</td>
<td>140.7</td>
<td>14.6</td>
<td>18.6</td>
<td>21.8*</td>
<td></td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>978</td>
<td>16</td>
<td>139.8</td>
<td>14.5</td>
<td>18.5</td>
<td>21.6**</td>
<td></td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>555</td>
<td>20</td>
<td>137.6</td>
<td>15.6</td>
<td>20.8</td>
<td>25.4*</td>
<td></td>
</tr>
<tr>
<td>In molds 1 day, water bath 1 day, at room temp., tested at room temp.</td>
<td>2 (lost 25 - 40% of wt. in water bath.)</td>
<td>140.4</td>
<td>16.0</td>
<td>18.6</td>
<td>14.5*</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>136.7</td>
<td>16.8</td>
<td>20.7</td>
<td>19.1*</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>133.2</td>
<td>18.3</td>
<td>23.4</td>
<td>22.0*</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>In molds 1 day, water bath 3 days at room temp., tested at 780°F.</td>
<td>2</td>
<td>5.5</td>
<td>552</td>
<td>12.5</td>
<td>140.7</td>
<td>15.4</td>
<td>18.1</td>
<td>14.5*</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>6.2</td>
<td>462</td>
<td>10.0</td>
<td>138.5</td>
<td>15.5</td>
<td>19.3</td>
<td>19.3*</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>5.5</td>
<td>362</td>
<td>9.5</td>
<td>137.6</td>
<td>15.5</td>
<td>20.9</td>
<td>25.5*</td>
</tr>
<tr>
<td>In molds 1 day, oven 1 day at 1300°F, tested at room temp.</td>
<td>2</td>
<td>1.5</td>
<td>2404</td>
<td>6</td>
<td>142.9</td>
<td>14.1</td>
<td>15.8</td>
<td>16.1*</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>1.3</td>
<td>1448</td>
<td>-</td>
<td>141.0</td>
<td>14.4</td>
<td>18.4</td>
<td>21.7*</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>1.3</td>
<td>1382</td>
<td>11</td>
<td>139.5</td>
<td>14.5</td>
<td>19.8</td>
<td>27.0*</td>
</tr>
<tr>
<td>In molds 1 day, room air 2 days, tested at room temp.</td>
<td>2</td>
<td>1.8</td>
<td>1479</td>
<td>15.0</td>
<td>146.6</td>
<td>12.6</td>
<td>15.4</td>
<td>17.9*</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>3.6</td>
<td>985</td>
<td>13.0</td>
<td>138.2</td>
<td>16.1</td>
<td>20.0</td>
<td>19.6*</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>3.0</td>
<td>1310</td>
<td>13.0</td>
<td>136.3</td>
<td>16.3</td>
<td>21.6</td>
<td>24.5*</td>
</tr>
<tr>
<td></td>
<td>0</td>
<td>1.3</td>
<td>4811</td>
<td>10.5</td>
<td>142.6</td>
<td>16.0</td>
<td>16.0</td>
<td>0*</td>
</tr>
<tr>
<td>0.5% CaCl₂</td>
<td>0</td>
<td>2.1</td>
<td>2572</td>
<td>13.5</td>
<td>166.6</td>
<td>13.5</td>
<td>14.0</td>
<td>0*</td>
</tr>
<tr>
<td>In molds 1 day, in air 3 days, immersed 1 day, tested at room temp.</td>
<td>2</td>
<td>2.3</td>
<td>1708</td>
<td>13.5</td>
<td>142.0</td>
<td>14.6</td>
<td>17.3</td>
<td>15.6*</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>2.8</td>
<td>1842</td>
<td>17.0</td>
<td>141.1</td>
<td>14.3</td>
<td>18.9</td>
<td>22.3*</td>
</tr>
<tr>
<td></td>
<td>3</td>
<td>2.8</td>
<td>2525</td>
<td>15.0</td>
<td>134.0</td>
<td>18.0</td>
<td>21.9</td>
<td>17.8**</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>3.0</td>
<td>1530</td>
<td>15.5</td>
<td>137.3</td>
<td>15.7</td>
<td>21.0</td>
<td>25.2*</td>
</tr>
<tr>
<td>In molds 1 day, room air 1 day, tested at room temp.</td>
<td>3</td>
<td>-</td>
<td>1026</td>
<td>14.0</td>
<td>138.2</td>
<td>15.5</td>
<td>19.5</td>
<td>20.5**</td>
</tr>
<tr>
<td>In molds 1 day, air 1 day, water bath 1 day, tested at room temp.</td>
<td>3</td>
<td>-</td>
<td>2525</td>
<td>10.0</td>
<td>134.0</td>
<td>18.0</td>
<td>21.9</td>
<td>17.8**</td>
</tr>
</tbody>
</table>

* Benson and Jessamine Limestone, Central Rock Co.

** Tyrone and Oregon Limestone, Boonesboro.
Most of the results shown in Table 2 were obtained from mixes composed of Jessamine and Benson limestones but some of the specimens (indicated by double astericks) were composed of Tyrone and Oregon limestones. Likewise, the gradations of the two aggregates differed somewhat in the coarser sizes. The two gradations were as follows:

<table>
<thead>
<tr>
<th>Sieve</th>
<th>% Passing</th>
<th>Sieve</th>
<th>% Passing</th>
</tr>
</thead>
<tbody>
<tr>
<td>1&quot;</td>
<td>100</td>
<td>1&quot;</td>
<td>100</td>
</tr>
<tr>
<td>3/4&quot;</td>
<td>85</td>
<td>3/4&quot;</td>
<td>100</td>
</tr>
<tr>
<td>3/8&quot;</td>
<td>65</td>
<td>1/2&quot;</td>
<td>80</td>
</tr>
<tr>
<td>No. 4</td>
<td>50</td>
<td>3/8&quot;</td>
<td>65</td>
</tr>
<tr>
<td>No. 10</td>
<td>37.5</td>
<td>No. 4</td>
<td>50</td>
</tr>
<tr>
<td>No. 16</td>
<td>31.5</td>
<td>No. 8</td>
<td>40</td>
</tr>
<tr>
<td>No. 40</td>
<td>22.5</td>
<td>No. 16</td>
<td>32</td>
</tr>
<tr>
<td>No. 50</td>
<td>20</td>
<td>No. 30</td>
<td>26</td>
</tr>
<tr>
<td>No. 100</td>
<td>12.5</td>
<td>No. 50</td>
<td>20.5</td>
</tr>
<tr>
<td>No. 200</td>
<td>10</td>
<td>No. 100</td>
<td>15.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td>No. 200</td>
<td>10</td>
</tr>
</tbody>
</table>

* Middle of Kentucky Spec.
** Corresponds to Fehr's No. 1 gradation (loc. cit.)

**Triaxial Test Series**

In order to compare the SS-1 mixes with "uncemented" mixes, in terms of cohesion and angle of internal friction; 4-in. diameter triaxial specimens were prepared with 3% SS-1, air-cured 6 days, and oven cured 1 day at 100°C before testing. The resulting values compared favorably with those obtained by Fehr (loc. cit.). A second set of specimens prepared and cured in the manner described above were immersed in water for 1 day prior to testing. These comparative data are as follows:

<table>
<thead>
<tr>
<th></th>
<th>3% SS-1 (dry)</th>
<th>3% SS-1 (soaked)</th>
<th>Fehr's No. 1 (dry, no cement added)</th>
</tr>
</thead>
<tbody>
<tr>
<td>C</td>
<td>20 psi</td>
<td>12 psi</td>
<td>19 psi</td>
</tr>
<tr>
<td>θ</td>
<td>45°</td>
<td>2°</td>
<td>55.30°</td>
</tr>
<tr>
<td>M.C.(%)</td>
<td>0.45</td>
<td>5.10</td>
<td>1.68</td>
</tr>
<tr>
<td>Voids (%)</td>
<td>14.47</td>
<td>14.46</td>
<td>10.3</td>
</tr>
</tbody>
</table>
Comparison of SS-1 Mixes with P.C. Mixes by Freeze-Thaw (Marshall-Type Specimens)

Marshall-type specimens were prepared with the Jessamine and Benson aggregate and 3% SS-1, air-cured for a nominal period of 28 days, immersed in water for 1 day, and then subjected to freezing and thawing. Concurrently, similar specimens containing portland cement in the approximate proportions of a 3-bag mix were moist-cured 28 days, immersed for 1 day, and subjected to freeze-thaw. Fig. 4 graphically compares the two types of mixes from the standpoint of gain or loss in weight attending successive freeze-thaw cycles.
- 3% SS-1, Air-Cured 28 Days, Soaked 1 Day before beginning F & T.
- 3-Hag Mix, P.C., Moist-Cured 28 Days, Soaked 1 Day.

Fig. 4: Graph Showing Comparatively the Loss in Weight of DGA Mixes Subjected to Freeze-Thaw
DISCUSSION

Although the tests and results described were somewhat cursory and exploratory in nature, several general observations pertinent to the potential use of these materials may be made. For instance, none of the non-air-entrained portland cement mixes appears to have sufficient durability (resistance to F & T) to permit their use in exposed roadway surfacing. However, this should not prevent their use in the construction of bases, provided that they are overlain by sufficient thicknesses of other insulating pavement. This observation, of course, applies equally to the "slump" and "no slump" mixes. Since it was impossible to entrain significant amounts of air or to obtain a satisfactory surface finish in mixes prepared at optimum moisture contents and was possible only by resorting to a special mixing technique to entrain air in the "near-slump" mixes, the only mix that appears to be suitable for service as a pavement surface is the normal air-entrained slump-type mix. This, of course, would require the use of forms in construction, and any advantage that the DGA concrete might have over ordinary air-entrained lean concrete using conventional coarse aggregates would probably arise from the comparative costs of the two types of aggregates. The minimum practicable cement factor from the standpoint of durability appears to be 3 bags per cu. yd.

With regard to the SS-1 mixes, it does not appear that any extraneous difficulties would be encountered in placing and compacting the material on the road, with the possible exceptions that might arise from premature drying during hot, dry weather or from extreme moisture conditions caused by severe rainy weather. It is anticipated that SS-1 mixes of this type might find their most advantageous use in bases protected by other pavement surface courses of sufficient quality to prevent raveling under traffic.