Remote Recession Sensing of Ablative Heat Shield Materials

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6th Ablation Workshop
April 10-11 2014, University of Illinois at Urbana-Champaign

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Outline:
- Motivation and Introduction
- The mARC facility
- Sample Geometry and Seeding Procedure
- Optical Set-up and Results
- Conclusions and future plans
• Current technologies for Thermal Protection Systems (TPS) often involve ablative materials.
• One successful example is Phenolic Impregnated Carbon Ablator (PICA, e.g. on Stardust or MSL).
• Surface recession of the ablator is one of the main performance parameters influencing
  - heat load to the inside
  - shape changes (aerothermodynamics)
  - structural integrity
• Currently, recession measurements usually are done after testing or flight → integrated recession over test/entry time
• To validate modeling, time resolved in situ measurements would be beneficial.

Ablative material response to a reentry heat flux: simplified sketches of two possible models and postflight SEM micrographs of the Stardust TPS

Introduction and Motivation
Flight data during Stardust Reentry Observation

- Major emission sources:
  - Strong continuum emission from hot surface
  - Post-shock plasma (O, N,N2+)
  - Ablating PICA (CN, C)

- In the observation data, additional emission was seen from:
  - Ca, Ca+ (recently found to be part of the carbon fiber form)
  - Zn from the white paint layer
  - Na, K, assigned to impurities in the phenolic resin from the curing process and also seen during ground testing

- These signatures due to impurities stood out clearly against the plasma and surface emission ➔ diffusion of boundary layer species into the post shock region ➔ strong emission.

→ Idea for recession measurements:
- Bury tracer elements at a defined depth inside the TPS
  ➔ once the recession reaches this depth, the tracer elements diffuse into the post-shock layer, start emitting at defined wavelengths and can be detected with emission spectroscopy.

Optical Recession/char-depth Sensor

Tracer element (Coating/paint)

Multiple materials ➔
• Multiple locations ➔ spatial information w/o optical spatial res.
• Multiple depths ➔ Time trace

Possible candidates
• Al (paint/powder/coating)
• Cu (not for arc jet testing)
• Cs, Li, Mg … (everything with strong emission lines)
• Low melting point or part of phenolic ➔ char depth sensor (e.g. Al)
• Higher melting point or sublimation ➔ recession sensor (e.g. Mg)

Application to arc-jet testing or re-entry observation
Optical Recession/Char-depth Sensor

- Tracer element (Coating/paint)
  - Mounted from the back: backside TC possible
  - Mounted from the front: no impact to TPS integrity

- Tracer plug (e.g. PICA)

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**Goals of this work** – demonstration of feasibility of the principle through testing in the NASA Ames mArc facility.
The NASA Ames mARC Facility

- subscale segmented arc heater, 30kW, up to 200 A DC
  - for this campaign operated at 70 A
- flow rate 0.45 g/s of air
- cooled thoriated tungsten tipped cathode, water-cooled copper anode
- 1.3 cm diameter constricted arc column channel followed by a
  converging-diverging nozzle (1 cm exit diameter)
  → plasma column approximately 1.3 cm in diameter
- cylindrical vacuum chamber of approximately 0.61 m in length and 0.3 m diameter
- chamber background pressures consistently approximately 2.67 kPa (20 Torr)

Calibration runs were performed to obtain stagnation heat flux at the test location at 5mm distance to the nozzle by using a 4.76 mm (0.187 inch) diameter hemispherical water-cooled Gardon Gage.

- Due to the high heat fluxes, the Gardon Gage exposure time was chosen to ~0.15 s while data was continuously acquired.

Plasma Conditions – Calibration Runs

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- Due to the high heat fluxes, the Gardon Gage exposure time was chosen to ~0.15 s while data was continuously acquired.
- Repeatability of the measured heat fluxes between different runs was quite good.
- Uncertainty of the measured heat fluxes estimated to ±10% → average value of the calibration runs of 2575 W/cm² used.

Sample calorimeter output for heat flux evaluation.

<table>
<thead>
<tr>
<th>Test #</th>
<th>Heat Flux [W/cm²]</th>
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<tr>
<td>1</td>
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Summary of stagnation heat flux for calibration runs.

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  → average value of the calibration runs of 2575 W/cm² used.
- This value is the heat flux to a hemispherical surface with a radius of 2.38 cm.
- The heat flux to the flat face material sample (8.38 cm square) follows from the relations given by Zoby and Sullivan:

\[
\dot{q}_{BB} = \dot{q}_{Hemi} \sqrt{\frac{r_{Hemi}}{r_{BB}}} = 2575 \sqrt{\frac{2.38}{14.7}} \frac{W}{cm^2} = 1036 \frac{W}{cm^2}
\]

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Summary of stagnation heat flux for calibration runs.

From the total recession of the sample and the test time of 10s, an average total recession rate was calculated. The total recession varied over the surface, though.

At the center of the sample the recession was mostly constant with highest recession values of about 0.056 cm/s for the test with emission spectroscopy measurements.

Seeding materials considered were metals, oxides and salts of Al, Ti, Mg and Si. Due to limited test time not all materials were evaluated in the mARC facility. The results presented focus on samples seeded with NaCl and MgCl.

The PICA coupons were drilled at given locations and the seeding rods (extruded with a polymer matrix) were inserted into the PICA and sealed using a PICA like paste allowing the seeding material to be encapsulated within the PICA.
Optical set-up

- Focal point imaging system with a 50 mm spherical mirror, focal length 305 mm → mostly collimated beam with the mirror diameter.
- The light was focused on a 200mm optical fiber and detected with an miniaturized spectrometer (Avantes AvaSpec-3648-USB2-UA, nominal wavelength range 180-1100nm).
- The f-number of the fiber (numerical aperture $n_A=0.22$) was matched using an aperture between mirror and fiber.
- The beam cross section covered the arc-jet nozzle exit with its upper edge, the virgin sample surface placed approximately at 10mm from the upper edge of the detection beam.
Results: spectra with test time

- During recession, the surface did move through the beam center towards the lower edge.
  - at different times, different parts of the sample surface were visible for the spectrometer
- With test time, increasing continuum radiation detected.
  - Absolute intensity not considered appropriately calibrated and is not the primary information …
- The measured spectra show continuous emission from the glowing sample, CN emission from ablation products interacting with the post-shock plasma and emission lines due to the seeding material (NaCl and MgCl).
- Emission lines of Mg (280nm, 285nm, and 518nm) and Na (568nm, 589nm, and 819nm) were identified in the arc-jet plasmaby a comparison with synthetic spectra at 9000K (arbitrarily chosen) based on NIST data using Boltzmann distributions.

Selected emission spectra for increasing test time

Measured spectra in comparison to NIST data.
Results: time trace of seeding emission

- All identified lines started showing up about 1 second after sample insertion and disappeared at roughly 4 seconds.
- The Na line at 589 nm was present right after sample insertion but disappeared together with the other emission lines (residual Na from the ambient air or on the sample surface?).
- Diameter of the seeding rod (1.5 mm) is chosen as thickness of the seeding layer
- Time for Mg emission (518 nm) >20% of max: $\Delta t=2.4$ s $\rightarrow$ recession rate 0.66 mm/s
  First and last appearance of Mg emission: $\Delta t=3.5$ s $\rightarrow$ recession rate 0.44 mm/s
  recession rate from total recession in the center region of the sample 0.5 to 0.6 mm/s

Time trace of spectrally integrated line emission of sodium and magnesium

Results

- Taking into account the limited performance of the mARC facility (beam profile, beam diameter, Mach number) → reasonable agreement with data from testing in the large arc-jet facilities.

Recession rates of PICA during mArc testing compared to data obtained in the NASA Ames IHF arc-jet facility vs. sample temperature

Conclusions

- The feasibility tests for this method are considered successful although testing under more controlled conditions is recommended for a further characterization.

- The recession rates determined from the emission spectroscopy measurements agree well with recession rates determined from absolute recession measurements of the material samples during this test campaign.

- An application for ground testing but more important for in-flight applications during real re-entry flight seems promising.

- Since spatial resolution is obtained through the location of the seeding material in the heat shield, the optical system does not need to happen spatially resolved (either through on-board or external observation).

- An extension of the sensor to a char depth sensor seems possible through a choice of seeding materials with lower melting/evaporation point, which then would be evaporated with the pyrolysis gases once the pyrolysis zone reaches the seeding depth.
Thanks for your attention!

Open for

Questions?
Results: spectra with test time

- During recession, the surface did move through the beam center towards the lower edge. 
  → at different times, different parts of the sample surface were visible for the spectrometer

- Spectrometer sensitivity across the field of view showed slight variations during pre-tests assigned to inhomogeneities of mirror and fiber
  → the same emission at different locations in the field of view might yield a different instrument response.
Results

- To get an estimate of the sample temperature, Planck radiation was calculated.
- By fitting the spectral shape (with $\varepsilon=0.9$), an average temperature was obtained.
- At the beginning of the test (3s after insertion), 2500K Planck radiation fits the measured spectra best, at the end (10s after insertion), this value increases to about 2750K.

Measured spectra at 3 and 10 seconds after sample insertion in comparison to Planck radiation at temperatures between 2400 K and 2900 K on linear scale. All spectra are normalized to the emission between 600 nm and 700 nm.
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- Since the spectrometer view angle provides only an obstructed view on the front surface (getting better with the surface recessing), this temperature is considered a lower bound for the actual front surface temperature.

Measured spectra at 3 and 10 seconds after sample insertion in comparison to Planck radiation at temperatures between 2400 K and 2900 K on log scale. All spectra are normalized to the emission between 600 nm and 700 nm.
Optical Emission Spectroscopy (OES): Set-up during SPRITE testing

- Emission spectroscopy measurements conducted to identify radiating species
- Two fiber coupled spectrometers used (200nm – 950nm) with focusing mirror
- Before test, optical paths close to each other barely touching the SPRITE nose tip
- Alignment before evacuation through a laser fed to the fibers

- Material recession would change the measurement position relative to the surface
- Continuous data acquisition during SPRITE and calorimeter insertion
  repetition rate ~2Hz $\rightarrow$ 81 spectra for the PICA model, 4 spectra for the calorimeter

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At the end of the model insertion (50s), spectra are qualitatively similar to the ones in front of the copper calorimeter → no effect from ablation, outside BL
Atom lines from Cu, O, N, molecular emission from N$_2$ and N$_2^+$
Shortly after insertion, emission peaks
Continuum emission seen → surface radiation
Additional atom emission from Ca, K and Na (also seen during Stardust observation)

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OES: Acquired Data – UV-spectra

- Difference between end and start of insertion should characterize the effect of ablation.
- Identified species: NH and OH, CN (strongly overlapping with N$_2^+$)

Conclusions:
- The ablation products OH, NH, and CN were seen in emission from the post shock/boundary layer
- Further characterization (e.g. for CH) requires experiments in higher spectral resolution.
- The role of K and Na as strong atom emissions is still to be verified, H was not seen.
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