12-3-1996

Binary Ferrihydrite Catalysts

Gerald P. Huffman  
*University of Kentucky, gphuffman@uky.edu*

Jianmin Zhao  
*University of Kentucky*

Zhen Fang  
*University of Kentucky*

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Recommended Citation  
Huffman, Gerald P.; Zhao, Jianmin; and Fang, Zhen, "Binary Ferrihydrite Catalysts" (1996). *Chemical and Materials Engineering Faculty Patents*. 28.  
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Primary Examiner—Asok Pal
Assistant Examiner—Bekir L. Yildirim
Attorney, Agent, or Firm—King and Schickli

ABSTRACT

A method of preparing a catalyst precursor comprises dissolving an iron salt and a salt of an oxoanion forming agent, in water so that a solution of the iron salt and oxoanion forming agent salt has a ratio of oxoanion/Fe of between 0.0001:1 to 0.5:1. Next is increasing the pH of the solution to 10 by adding a strong base followed by collecting of precipitate having a binary ferrihydrate structure. A binary ferrihydrate catalyst precursor is also prepared by dissolving an iron salt in water. The solution is brought to a pH of substantially 10 to obtain ferrihydrate precipitate. The precipitate is then filtered and washed with distilled water and subsequently admixed with a hydroxy carboxylic acid solution. The admixture is mixed/agitated and the binary ferrihydrate precipitate is then filtered and recovered.

16 Claims, 1 Drawing Sheet
Iron ion in the interior

Iron ion at the surface

Fig. 1b

Fig. 1c

Interior

Surface

d = 30A

Fig. 1a
This invention was made with government support under contract number DE-FC22-90PC90029 awarded by the Department of Energy. The government has certain rights in the invention.

TECHNICAL FIELD

The present invention relates generally to the field of catalysis and more particularly, to a method of producing highly dispersed iron oxide catalyst precursors useful for direct coal liquefaction and to these catalyst precursors and catalysts produced therefrom useful for direct coal liquefaction.

BACKGROUND OF THE INVENTION

Coal liquefaction is the process of converting various ranks of coal, including lignite, subbituminous, and bituminous, to petroleum-like hydrocarbon liquids. These liquids contain less sulfur, nitrogen, and ash than the solid starting material and are also easier to transport and utilize. Advantageously, the resulting hydrocarbon liquids are suitable for utilization as refinery feed stocks for the manufacture of, for example, gasoline; jet, diesel and turbine fuels; heating and fuel oils; and other petro-chemical products that may be utilized to meet commercial, residential and industrial fuel requirements.

The coal liquefaction process involves depolymerizing the coal and increasing the ratio of hydrogen to carbon atoms by a factor of from about two to three times that in the starting coal materials. In direct coal liquefaction (DCL), the hydrogen is chemically added to the coal molecules under conditions of high pressure and temperature.

More specifically, in DCL, the coal is first crushed and slurred. Preferably, the slurry is made utilizing a process-derived solvent. A catalyst is then added and/or the solvent may be hydrogenated to improve hydrogen transfer to the coal. The slurry is then heated to, for example, 400°-500° C. and pressurized under hydrogen to a pressure of 140-300 atm. As the coal is heated to the desired reaction temperature and held there for the necessary residence time, chemical bonds are broken and free-radical fragments are generated. These free-radical fragments may then participate in various secondary reactions, for example, reacting further to form lighter liquids, polymerizing to form high-molecular weight compounds or combining with hydrogen to produce stable liquids. By controlling these secondary reactions it is possible to achieve high conversion rates and good selectivity to produce desired, distillable liquid products.

The same basic procedures may be used to liquify other hydrocarbon-based solids such as waste plastics and rubber tires and to colliquefy mixtures of coal with such waste materials. The catalysts described in this patent can also be used for these processes. For the sake of simplicity, the liquefaction process for all such materials will be generally referred to as "direct coal liquefaction" or DCL.

An important factor in the conversion efficiency and yield of any DCL process is the material utilized to catalyze the process. In order to improve processing efficiency a variety of novel techniques have been utilized in the past to produce highly dispersed iron oxide catalyst precursors. These iron oxide catalyst precursors are often reacted with sulfur during liquefaction to provide a catalyst for DCL processing. Under the high pressure and temperature conditions of the DCL process, many iron oxide catalysts undergo phase transfor-

mations to Fe₁₋ₓS. A good DCL iron oxide catalyst precursor must be able to maintain its dispersion and transform to a highly dispersed Fe₁₋ₓS phase under DCL reaction condition.

SUMMARY OF THE INVENTION

Accordingly, two primary objectives of the present invention are to provide a new and improved DCL catalyst having the above-described advantages and a simple and efficient method for producing the same.

The present invention provides a method for producing an improved catalyst precursor having a binary ferrhydrite structure that advantageously resists agglomeration at temperatures and pressures associated with the DCL process. Accordingly, the catalyst precursor transforms to a dispersed and catalytically active Fe₁₋ₓS phase so as to allow more efficient conversion and increased yields of desired liquid products.

Yet another object of the present invention is to provide a method of producing a catalyst precursor by means of a simple precipitation method that incorporates iron as the major cation and that includes a secondary agent which contains an element from the group consisting of tin, aluminum, silicon, molybdenum, phosphorus, boron, chromium, manganese and tungsten. Alternatively, a catalyst precursor may be prepared by admixing ferrhydrite with an hydroxy-carboxylic acid solution and collecting the precipitate. Advantageously, the resulting catalyst exhibits substantially less particle agglomeration under DCL reaction conditions.

Additional objects, advantages and other novel features of the invention will be more readily apparent from the appended claims.
be collected by filtering. Once it is collected the precipitate is washed and filtered repeatedly with distilled water until a pH of 7 is reached. The collected precipitate is then dried whereupon it is ready for use as a catalyst precursor in DCL processes. Advantages of, when reacted with a sulfur donor such as dimethyl disulfide, the binary ferricyridate catalyst precursor converts to a dispersed and catalytically active phase of Fe₃₋S under DCL reaction conditions providing greater conversion efficiency and higher overall yields.

In some types of DCL or other hydrotreatment processes, however, it may be desirable to leave the catalyst in an oxidized form; this can be accomplished by not adding sulfur or by adding catalyst in concentrations that exceed the sulfur level.

It should further be appreciated that anions of hydroxy-carboxylic acids may also be used as the oxoanion agents (RO₂⁻). Such hydroxy-carboxylic acids include citric acid, meso tartaric acid, L-tartaric acid, glycolic acid, salicylic acid, DL-malic acid and mucic acid. The hydroxy-carboxylic acid is dissolved in a second aqueous solution and is added to a ferricyridate precipitate to form a surface modified binary ferricyridate precipitate. This is then collected for subsequent use as a catalyst precursor. The average particle size of the precipitated catalyst precursor of either method is less than 100 Å.

**BRIEF DESCRIPTION OF THE DRAWING FIGURE**

The accompanying drawing incorporated in and forming a part of the specification, illustrates several aspects of the present invention and together with the description serves to explain the principles of the invention. In the drawing:

**FIG. 1a-c are a schematic representation of the catalyst precursor of the present invention including chemisorbed oxoanions on its surface.**

**DETAILED DESCRIPTION OF THE INVENTION**

As indicated above, the present invention relates to a method of preparing a catalyst precursor of binary ferricyridate structure. Advantageously, when reacted with a sulfur donor the catalyst precursor converts to a dispersed Fe₃₋S phase that is catalytically active and therefore useful in DCL processing wherein various ranks of coal and/or other hydrocarbon materials such as waste plastics and rubber tires are converted to petroleum-like hydrocarbon liquids.

The method includes the step of dissolving an iron salt in a first aqueous solution. Iron is the active agent cation for the catalyst. Preferably, the iron is in its ferric (Fe III) form. Any number of ferric salts may be utilized including various anions such as nitrates, sulfates and chlorides. Preferably, Fe₂(SO₄)₃(CH₃COO)₂•2H₂O, Fe₂(SO₄)₃•9H₂O, FeCl₃•6H₂O and more preferably Fe(NO₃)₃•9H₂O are utilized and dissolved in the first aqueous solution.

A separate, second aqueous solution is then prepared by dissolving a salt of an oxoanion forming agent in distilled water. The oxoanion forming agent produces oxoanions (MO₂⁻) in water. The element M of the oxoanion is preferably selected from a group consisting of silicon, molybdenum, phosphorous, boron, chromium, manganese, tungsten and any mixtures thereof. Next is the admixing of the first and second solutions. The concentration of the iron salt and salt of the oxoanion forming agent utilized in the first and second solutions are such as to provide an atomic ratio of M/Fe and a ratio of oxoanion/Fe between 0.0001:1 and 0.5:1 and more preferably between 0.01:1 to 0.1:1. Then, ammonium hydroxide or some other strong base is slowly added to the admixed solution (while mixing or agitating) to bring the admixed solution to a pH of about 10. This change in pH causes a binary ferricyridate product to precipitate. It is this precipitate that is collected (e.g. by filtering and drying) and utilized as a catalyst precursor.

Preferably, the salt of the oxoanion forming agent utilized in the present method is selected from a group consisting of Na₂SiO₃•9H₂O, K₂SiO₃, Na₂ xSiO₃ (where x=3-5), K₂Si₅O₁₇•H₂O, Na₂Si₅O₁₇, K₂Si₅O₁₇, (NH₄)₂MoO₄•2H₂O, 3(NH₄)₂SO₄•2H₂O, 2MoO₃•6H₂O, Na₂MoO₄•2H₂O, K₂MoO₄•2H₂O, Na₂MoO₄•2H₂O, K₂O•3MoO₃•2H₂O, Na₂MoO₄•13•6H₂O, K₂O•3MoO₃•3H₂O, Na₂HPO₄, NaH₂PO₄, 2H₂O, Na₂HPO₄•5H₂O, Na₂H₂PO₄•H₂O, Na₂P₂O₇•10H₂O, K₂P₂O₇•3H₂O, NaNH₄HPO₄•4H₂O, NaBO₂•4H₂O, KBO₂•10H₂O, K₂B₂O₅•8H₂O, Na₂Cr₂O₇•2H₂O, K₂Cr₂O₇•2H₂O, Na₂Cr₂O₇•10H₂O, K₂Cr₂O₇, (NH₄)₂Cr₂O₇, Na₂MoO₄•10H₂O, K₂MoO₄•10H₂O, Na₂MoO₄, NaN₂MoO₄, NaN₂MoO₄, (NH₄)₂Mo₆W₈O₄₀ and any mixtures thereof.

Alternatively, a binary ferricyridate catalyst precursor may be prepared by dissolving iron salt (Fe²⁺) such as Fe(NO₃)₃•9H₂O, Fe₂(SO₄)₃(CH₃COO)₂•2H₂O, Fe₂(SO₄)₃•9H₂O and FeCl₃•6H₂O in water (preferably distilled water) to form an iron salt solution. Next is the adjusting of the pH of the iron salt solution to substantially 10. This may be done by slowly adding ammonium hydroxide or other strong base. As the pH slowly approaches 10, a ferricyridate precipitate is produced. This ferricyridate precipitate is washed with distilled water until a pH of 7 is reached. The ferricyridate precipitate is then added to a hydroxy-carboxylic acid solution including a hydroxy-carboxylic acid selected from a group including citric, meso tartaric, L-tartaric, glycolic, salicylic, DL-malic, mucic and any mixtures thereof. The solution has a molar concentration of hydroxy-carboxylic acid of between 10⁻⁴ to 10⁻⁸ M. After mixing, the admixed solution is filtered to collect a binary ferricyridate precipitate that may then be washed with distilled water and dried for subsequent use. In this approach the various hydroxy-carboxylic acids form the oxoanions (RO₂⁻).

The catalyst precursor product of both of the above described methods is characterized by a ratio of oxoanion/Fe typically between 0.0001:1 and 0.5:1 and more preferably 0.01:1 to 0.1:1. Further, after reaction of the resulting precursor with a sulfur donor (e.g. dimethyl disulfide), an Fe₃₋S active phase is formed. This characteristic makes the catalyst product of the present invention particularly useful for the efficient and effective processing of coal or other hydrocarbon materials by DCL.

It is well established that the performance of an iron oxide catalyst is determined mainly by its surface structure and condition. Ferricyridate is one of the eight major iron oxide/oxyhydroxide compounds. While its specific structure is still controversial, we have found using x-ray absorption fine structure spectroscopy that the structure is oxyhydroxide-like. More significantly, at the surface the catalyst a large percentage of iron ions are at coordinate unsaturated (CUS) sites. These CUS sites play a major role in controlling particle agglomeration and phase transformation from the ferricyridate to α-Fe₂O₃ at high temperature in air.

Studies described in the examples to follow have shown that the particle agglomeration and phase transition properties of conventional ferricyridate catalysts and the binary
ferricydrite catalyst of the present invention are both dependent upon the surface structure and the surface conditions. Being coordinate unsaturated, the CUS sites at the surface of a conventional ferricydrite catalyst are susceptible to absorbing water molecules. The absorbed water molecules link the small ferricydrite particles into clusters. At elevated temperatures and in air, the water molecules are evolved from the particle joints, leading to particle agglomeration and phase transition to α-Fe₂O₃. Accordingly, under DCL conditions, a conventional ferricydrite catalyst disadvantageously suffers from converting to a low surface area Fe₃₋₅S phase when subjected to high pressure and temperature conditions characteristic of DCL processing.

Stated another way, the CUS sites with absorbed water on the ferricydrite catalyst surface may be viewed as crystal growth sites. In contrast, in the binary ferricydrite catalysts of the present invention, oxoanions (MO₆⁻ or RO₇⁻) are present during precipitation and many of the CUS sites incorporate the oxoanions instead of water thereby forming a chemisorbed oxoanion-iron (M—O—Fe or R—O—Fe) complex at the surface (note FIG. 1). Advantageously, it should be appreciated that the presence of the oxoanion effectively blocks a substantial percentage of the crystal growth sites thereby resulting in a reduction in agglomeration.

As a result of this activity, phase transformation is resisted and an increased surface area of Fe₃₋₅S phase for catalytic activity is formed during DCL reaction. This advantageously results in more efficient and effective direct coal liquefaction, leading to higher yields and lower processing costs.

The following synthesis and examples are presented to further illustrate the invention, but it is not to be considered as limited thereto.

**EXAMPLE 1**

Preparation of Silicon—Ferricydrite Catalyst

40.4 grams of an Fe(NO₃)₃·9H₂O was added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 1.42 grams of Na₂SiO₃ was added to 50 mL of distilled water in a smaller beaker. After the Na₂SiO₃ was completely dissolved, the solution was poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of Si/Fe or ratio of oxoanion/Fe of 0.05:1. Subsequently, ammonium hydroxide was slowly added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide was then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution was changed from gold to dark reddish brown. The solution was vigorously stirred for another 10 minutes. The precipitate was then filtered and washed repeatedly with distilled water until the filtrate showed a pH of 7. The precipitate cake was then oven dried at 50°C and ground into a fine powder. Before use, it was vacuumed dried at 130°C for 3 hours.

**EXAMPLE 2**

Preparation of Molybdenum—Ferricydrite Catalyst

40.4 grams of an Fe(NO₃)₃·9H₂O was added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 6.08 grams of (NH₄)₆Mo₇O₂₄·4H₂O was added to 50 mL of distilled water in a smaller beaker. After the (NH₄)₆Mo₇O₂₄·4H₂O was completely dissolved, the solution was poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of Mo/Fe or ratio of oxoanion/Fe of 0.05:1. Subsequently, ammonium hydroxide was slowly added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide was then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution was changed from gold to dark reddish brown. The solution was vigorously stirred for another 10 minutes. The precipitate was then filtered and washed repeatedly with distilled water until the filtrate showed a pH of 7. The precipitate cake was then oven dried at 50°C and ground into a fine powder. Before use, it was vacuumed dried at 130°C for 3 hours.

**EXAMPLE 3**

Preparation of Phosphorous—Ferricydrite Catalyst

40.4 grams of an Fe(NO₃)₃·9H₂O was added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 1.72 grams of Na₃PO₄ was added to 50 mL of distilled water in a smaller beaker. After the Na₃PO₄ was completely dissolved, the solution was poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of P/Fe or ratio of oxoanion/Fe of 0.05:1. Subsequently, ammonium hydroxide was slowly added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide was then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution was changed from gold to dark reddish brown. The solution was vigorously stirred for another 10 minutes. The precipitate was then filtered and washed repeatedly with distilled water until the filtrate showed a pH of 7. The precipitate cake was then oven dried at 50°C and ground into a fine powder. Before use, it was vacuumed dried at 130°C for 3 hours.
5,580,839

EXAMPLE 6
Preparation of Phosphorous—Ferrhydrite Catalyst

4.04 grams of an Fe(NO₃)₃·9H₂O is added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 3.44 grams of Na₂HPO₄ is added to 50 mL of distilled water in a smaller beaker. After the Na₂HPO₄ is completely dissolved, the solution is poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of P/Fe of 0.1:1. Subsequently, ammonium hydroxide is added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution is changed from gold to dark reddish brown. The solution is vigorously stirred for another 10 minutes. The precipitate cake is then filtered and washed repeatedly with distilled water until the filtrate shows a pH of 7. The precipitate cake is then oven dried at 50°C and ground into a fine powder. Before use, it is vacuumed dried at 130°C for 3 hours.

EXAMPLE 7
Preparation of Boron—Ferrhydrite Catalyst

4.04 grams of an Fe(NO₃)₃·9H₂O is added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 4.58 grams of NaBO₂·4H₂O is added to 50 mL of distilled water in a smaller beaker. After the NaBO₂·4H₂O is completely dissolved, the solution is poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of B/Fe or ratio of oxoamion/Fe of 0.05:1. Subsequently, ammonium hydroxide is slowly added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide is then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution is changed from gold to dark reddish brown. The solution is vigorously stirred for another 10 minutes. The precipitate is then filtered and washed repeatedly with distilled water until the filtrate shows a pH of 7. The precipitate cake is then oven dried at 50°C and ground into a fine powder. Before use, it is vacuumed dried at 130°C for 3 hours.

EXAMPLE 8
Preparation of Chromium—Ferrhydrite Catalyst

4.04 grams of an Fe(NO₃)₃·9H₂O is added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 0.63 grams of (NH₄)₂Cr₂O₇ is added to 50 mL of distilled water in a smaller beaker. After the (NH₄)₂Cr₂O₇ is completely dissolved, the solution is poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of Cr/Fe or ratio of oxoamion/Fe of 0.02:1. Subsequently, ammonium hydroxide is added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide is then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution is changed from gold to dark reddish brown. The solution is vigorously stirred for another 10 minutes. The precipitate is then filtered and washed repeatedly with distilled water until the filtrate shows a pH of 7. The precipitate cake is then oven dried at 50°C and ground into a fine powder. Before use, it is vacuumed dried at 130°C for 3 hours.

EXAMPLE 9
Preparation of Manganese—Ferrhydrite Catalyst

4.04 grams of an Fe(NO₃)₃·9H₂O is added to one liter of distilled water in a two liter glass beaker while being subjected to magnetic stirring. Separately 2.98 grams of Na₂MnO₄·3H₂O is added to 50 mL of distilled water in a smaller beaker. After the Na₂MnO₄·3H₂O is completely dissolved, the solution is poured in the Fe(NO₃)₃·9H₂O solution to form an admixed solution with an atomic ratio of Mn/Fe or ratio of oxoamion/Fe of 0.08:1. Subsequently, ammonium hydroxide is slowly added to the solution to bring the pH to 9 with constant stirring. Additional ammonium hydroxide is then added drop wise to increase the pH to 10 with constant checking of the pH. During this time the solution is changed from gold to dark reddish brown. The solution is vigorously stirred for another 10 minutes. The precipitate is then filtered and washed repeatedly with distilled water until the filtrate shows a pH of 7. The precipitate cake is then oven dried at 50°C and ground into a fine powder. Before use, it is vacuumed dried at 130°C for 3 hours.

EXAMPLE 10
27.03 grams of FeCl₃·6H₂O are substituted for the 40.4 grams of Fe(NO₃)₃·9H₂O in Examples 1–10.

EXAMPLE 11
28.01 grams of Fe₂(OH)₃·9H₂O are substituted for the 40.4 grams of Fe(NO₃)₃·9H₂O in Examples 1–10.

EXAMPLE 12
90.03 grams of Fe₃(SO₄)₂(NH₄)₂SO₄·24H₂O are substituted for the 40.4 grams of Fe(NO₃)₃·9H₂O in Examples 1–10.

EXAMPLE 13
Preparation of Citric Acid—Ferrhydrite Catalyst

4.04 gram Fe(NO₃)₃·9H₂O was added to one liter of distilled water in a two liter glass beaker while undergoing magnetic stirring. Ammonium hydroxide was slowly added to this solution to bring the pH to 10 with constant stirring. During this time the solution was changed from gold to dark reddish brown. The precipitate was filtered and washed repeatedly with distilled water and was subsequently admixed with 50 ml of citric acid solution containing 1–2
grams citric acid. The admix was stirred for 5 minutes and filtered. Finally the precipitate cake was oven dried at 50°C and ground into a fine powder. Before use it was vacuumed dried at 130°C for three hours.

EXAMPLES 14–19

Acetic, meso tartaric, L-tartaric, glycolic, salicylic, DL-malic and mucic acids are individually substituted for citric acid in Example 14.

Liquefaction test results for binary ferrhydrite catalysts made from the catalyst precursors treated with Si containing doping agent and citric acid as prepared per Examples 1 and 13 were directly compared with test results for a commercial catalyst of a ferrhydrite structure made from an iron carbonyl with flame synthesis method sold under the trademark NANOCAT and manufactured by Mach I, Inc. of King Of Prussia, Pa. This commercial ferrhydrite catalyst precursor is highly dispersed with a mean particle diameter of 30 Å and a surface area greater than 260 m²/g.

For purposes of these tests, transmission electron micrographs were obtained using a Hitachi H-1000 NASTEM System. The operating voltage was set at 200 kV. Several micrographs from different locations on the grid were taken at magnifications ranging from 50 k to 200 k.

Mössbauer spectra were recorded with a constant acceleration spectrometer. The radioactive source consisted of approximately 50 mCi of 57Co in Pd matrix. Because of the small particle sizes, the Mössbauer spectra exhibit significant superparamagnetic relaxation effect. In order to observe the magnetic hyperfine splitting, all spectra were recorded at 10K using an Air Products Displex cryogenic system.

X-ray diffraction measurements were performed on a Rigaku Dmax diffractometer using the Cu Kα emission line.

DECS-17 Blind Canyon Coal was used for the coal liquefaction experiments. The analysis of the coal sample is listed in Table 1.

<table>
<thead>
<tr>
<th>Elemental Analysis of Blind Canyon (DECS-17)</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Proximate, Dry Basis (%)</strong></td>
</tr>
<tr>
<td>Ash</td>
</tr>
<tr>
<td>Volatile</td>
</tr>
<tr>
<td>Fixed Carbon</td>
</tr>
<tr>
<td>Ultimate, Dry Ash Free Basis (%)</td>
</tr>
<tr>
<td>Carbon</td>
</tr>
<tr>
<td>Hydrogen</td>
</tr>
<tr>
<td>Nitrogen</td>
</tr>
<tr>
<td>Total Sulfur</td>
</tr>
<tr>
<td>Oxygen</td>
</tr>
</tbody>
</table>

A mixture of 5 grams of coal and iron catalyst precursor with Fe:coal=0.6% wt was used for each experiment. 1, 2, 3, 4-tetrahydrornaphthalene (1, 2, 3, 4-tetrahydrornaphthalene/coal=2/1 wt) along with dimethyl disulphide (DMDS) as a sulfur donor for the preparation of the iron catalyst from the precursor (S:precursor=2/1 wt) were also added to the reactor. After loading, the reactor was pressurized with hydrogen to 1000 psig at room temperature and agitated vertically to 400 cycles per minute for an hour in a fluid sand bath of 410°C.

After reaction, the gas was then removed from the cooled reactor and analyzed with gas chromatography. The rest of the products were analyzed using Soxhlet extraction. The definitions of the solubility classes used in this work (on a weight percent, dry-ash-free basis) are as follows (a) oils (pentaene soluble), (b) asphaltenes (toluene soluble, pentane insoluble), (c) preasphaltenes (THF soluble, toluene insoluble), and (d) insoluble organic matter (IOM). The reproducibility for determination of gas, oils, asphaltenes, preasphaltenes and total conversions are +/-0.2%, +/-2%, +/-2%, +/-1% and +/-2%, respectively.

The micrographs of the binary ferrhydrite catalyst precursors prepared in accordance with example 1 show heavy particle agglomeration, although fine nanoscale particles were discerned. Once the particle aggregate was focused on by the electron beam, the particles often spread and individual particles could be easily observed. The spreading force was the static electric Coulomb force induced by sample charging by the high intensity electron beam. The estimated average particle size for the Si-ferrhydrite catalyst precursor was 50 Å. The conventional ferrhydrite catalyst precursor had a particle size of approximately 30 Å and showed much less particle agglomeration. This explains why its bulk density is approximately 10 times less than that of the prepared binary ferrhydrite catalyst precursor.

The Mössbauer spectra of the prepared binary and conventional ferrhydrite catalyst precursors indicate that the structures of the catalyst precursors are essentially identical. The x-ray diffraction patterns for all the catalyst precursors show two broad peaks, typical for ferrhydrite. The peak positions for the conventional ferrhydrite and silicon-ferrhydrite catalyst precursors are the same.

In order to examine the phase transformation and agglomeration properties of the catalyst precursors, each of the conventional ferrhydrite as well as the silicon-ferrhydrite sample was subjected to 400°C annealing for 5 hours in air. X-ray diffraction patterns of the annealed samples were taken. The annealed conventional ferrhydrite catalyst precursor showed only an α-Fe₂O₃ phase. The color of the conventional ferrhydrite sample following annealing turned orange, giving a visual indication of the phase change. Using Scherrer’s equation, the average α-Fe₂O₃ particle size was estimated to be greater than 300 Å for the annealed conventional ferrhydrite catalyst precursor.

In contrast the x-ray diffraction patterns and colors for the silicon-ferrhydrite catalyst precursor remain essentially unchanged after annealing with only a trace of α-Fe₂O₃ seen in the silicon-ferrhydrite x-ray diffraction pattern. These results clearly show that the presence of the o xoanion at the surface significantly reduces and/or effectively prevents ferrhydrites from phase transformation to α-Fe₂O₃ and subsequent growth in particle size under annealing conditions.

Coal liquefaction tests were performed on the conventional ferrhydrite and silicon, and citric acid treated binary ferrhydrite catalyst precursors in the presence of a sulfur donor agent in a tubing bomb reactor in accordance with the processing parameters outlined above. Coal conversion was determined based upon the amount of THF-insoluble residual. The coal liquefaction results are presented in Table 2.
TABLE 2 DCL REACTION PRODUCTS ANALYSIS

<table>
<thead>
<tr>
<th>Catalyst</th>
<th>Oil</th>
<th>Gas</th>
<th>Asphaltene</th>
<th>Preasphaltene</th>
<th>Total</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal</td>
<td>31.2</td>
<td>2.4</td>
<td>37.6</td>
<td>9.5</td>
<td>80.7</td>
</tr>
<tr>
<td>Conventional</td>
<td>33.1</td>
<td>2.8</td>
<td>50.2</td>
<td>0.6</td>
<td>86.7</td>
</tr>
<tr>
<td>Ferrihydrite</td>
<td>35.7</td>
<td>3.1</td>
<td>42.6</td>
<td>5.0</td>
<td>86.4</td>
</tr>
<tr>
<td>Citric Acid/</td>
<td>36.8</td>
<td>2.9</td>
<td>42.3</td>
<td>2.5</td>
<td>84.5</td>
</tr>
</tbody>
</table>

The silicon-ferrihydrite and citric acid-ferrihydrite based catalysts showed both total yield and oil yield relative to reaction without catalyst and enhancements in oil yield relative to reaction with the conventional ferrihydrite based catalyst.

The invention has been described herein with reference to certain preferred embodiments. However, as obvious variations thereon become apparent to those skilled in the art, the invention is not to be considered as limited thereto.

We claim:

1. A method of preparing a catalyst precursor comprising the steps of:
   dissolving an iron salt and a salt of an oxoanion forming agent including an element (M) selected from a group consisting of silicon, molybdenum, phosphorous, boron, chromium, manganese, tungsten and any mixture thereof in water so that a solution of the iron salt and oxoanion forming agent salt has an atomic ratio of M/Fe and a ratio of oxoanion/Fe of between 0.0001 to 0.5;
   increasing the pH to 10 by adding a strong base to obtain ferrihydrite precipitate; and
   collecting precipitate of binary ferrihydrite structure.

2. The method set forth in claim 1, wherein said iron salt is selected from a group consisting of Fe(NO₃)₃·9H₂O, Fe₂(SO₄)₃·9H₂O, Fe₃(SO₄)₂·9H₂O, FeCl₃·6H₂O and any mixtures thereof.

3. The method set forth in claim 2, wherein said oxoanion forming agent is selected from a group consisting of Na₃SiO₃·9H₂O, K₂Si₃O₈, Na₂O·SiO₂ (where x=3-5), K₂Si₃O₈·H₂O, Na₂Si₃O₈, K₂Si₃O₈·(NH₄)₂Mo₇O₂₄·4H₂O, (NH₄)₂·O₅Mo₇O₂₄·2MoO₇·6H₂O, Na₂MoO₄·2H₂O, K₂MoO₄, Na₂MoO₄·2H₂O, K₂O·MoO₃·3H₂O, Na₂MoO₄·13·6H₂O, K₂O·MoO₃·3H₂O, Na₂HPO₄, K₂HPO₄, NaH₂PO₄·2H₂O, Na₂HPO₄·5H₂O, Na₂HPO₄·H₂O, Na₂P₂O₃·10H₂O, K₂P₂O₃·3H₂O, Na₂HPO₄·4H₂O, Na₂BO₄·4H₂O, K₂BO₂, Na₂B₂O₇·10H₂O, K₂B₂O₇·8H₂O, Na₂Cr₂O₇·2H₂O, K₂Cr₂O₇, Na₂Cr₂O₇·10H₂O, K₂Cr₂O₇·10H₂O, (NH₄)₂Cr₂O₇, Na₂MnO₄·10H₂O, K₂MnO₄, NaMnO₄, KMnO₄, (NH₄)₂·H₂W₁₄O₄₀ and any mixtures thereof.

4. The method set forth in claim 1, including washing the collected precipitate until a pH of 7 is reached.

5. The method set forth in claim 4, including drying the washed precipitate.

6. The method set forth in claim 1, including adding ammonium hydroxide to the solution to bring the pH to substantially 10 prior to collecting the precipitate.

7. A direct coal liquefaction catalyst precursor comprising a binary ferrihydrite structure of iron (Fe) and an oxoanion forming agent containing a secondary element (M) selected from a group consisting of silicon, molybdenum, phosphorous, boron, chromium, manganese, tungsten and mixtures thereof having an atomic ratio of M/Fe of between 0.0001 to 0.5 that has average particle size of less than 100 Å and further shows no particle agglomeration at temperatures of up to 400°C in air.

8. The catalyst precursor set forth in claim 7, having a ferrihydrite structure with an oxoanion-iron (M—O—Fe) species chemisorbed at the surface.

9. A catalyst prepared from the binary ferrihydrite precursor of claim 7 by reacting the precursor with a sulfur donor.

10. A method of preparing a catalyst precursor comprising the steps of:
   - dissolving an iron salt in water to form an iron salt solution;
   - adjusting the pH of the iron salt solution to between 6 and 10;
   - collecting a ferrihydrite precipitate;
   - adding the collected ferrihydrite precipitate to a hydroxy-carboxylic acid solution including a hydroxy carboxylic acid selected from a group consisting of citric, meso tartaric, L-tartaric, glycolic, salicylic, DL-malic, mucic acids and any mixtures thereof;
   - mixing the hydroxy carboxylic acid solution and ferrihydrite precipitate admixture;
   - filtering the admixture to collect a binary ferrihydrite precipitate product.

11. The method set forth in claim 10, wherein said iron salt is selected from a group consisting of Fe(NO₃)₃·9H₂O, Fe₂(SO₄)₃·9H₂O, Fe₃(SO₄)₂·9H₂O, FeCl₃·6H₂O and any mixtures thereof.

12. The method set forth in claim 10, including adding ammonium hydroxide to the iron salt solution to bring the pH to substantially 10 prior to collecting the ferrihydrite precipitate.

13. The method set forth in claim 10, including washing the collected ferrihydrite precipitate until a pH of 7 is reached.

14. A direct coal liquefaction catalyst precursor comprising a binary ferrihydrite structure of iron chemisorbed with an oxoanion of a hydroxy-carboxylic acid selected from a group consisting of citric, meso tartaric, L-tartaric, glycolic, salicylic, DL-malic, mucic acids and any mixtures thereof that has oxoanion-iron ratio of 0.0001 to 0.5, an average particle size of less than 100 Å.

15. A catalyst prepared from the catalyst precursor of claim 14 by reacting the precursor with a sulfur donor.

16. A method of preparing a catalyst precursor comprising the steps of:
   - preparing a binary ferrihydrite product by chemisorbing oxoamions with iron so as to provide an oxoanion-iron ratio of between 0.0001 to 0.5, said oxoamions being selected from a group consisting of MO₃⁻ and RO⁻ wherein M equals silicon, molybdenum, phosphorous, boron, chromium, manganese, tungsten and mixtures thereof and RO⁻ equal an anion of citric acid, acetic acid, meso tartaric acid, L-tartaric acid, glycolic acid, salicylic acid, DL-malic acid, mucic acid and mixtures thereof.